

EPS

Slewing Drives

Edition December 2011



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Applications



Civil Engineering



Material and working elevators



Shipboard and deck cranes



Tower cranes



Grab cranes



Container gantries


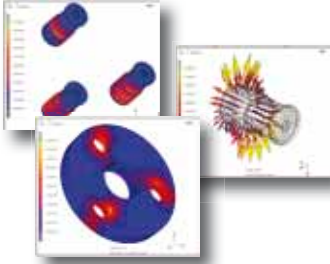

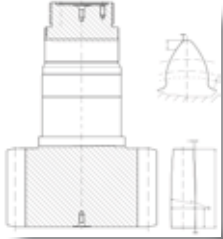
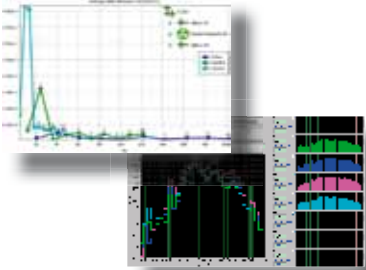



Yaw and pitch drives for wind turbines



Stacker and reclaimer

Features and Benefits

<ul style="list-style-type: none"> • Wide range of planetary gear reducers, from 1 300 to 145 000 N m torque • Modular design concept 		<ul style="list-style-type: none"> → Right choice of the drive and cost effective solution for final customer tailored solutions → Delivery flexibility and reliability
<ul style="list-style-type: none"> • Nodular cast iron housing and planet carrier, full complement needle roller bearings • ISO 12944 class paint on request • Grease and oil lubricant feasibility • Double seal and labyrinth options 		<ul style="list-style-type: none"> → Highest standards in construction materials, maximum load strength → Assuring the best coating for your drives → Suitability for application demand → Suitability for the most severe working conditions → Easy installation and maintenance
<ul style="list-style-type: none"> • Case hardened ground gears designed and rated according to DIN 3990 • Gears with ground finish • Efficient, precise and upgraded machine tools • Cutting edge industrial technology 		<ul style="list-style-type: none"> → Clear and reliable performances ratings → Performance, reliability, durability, long maintenance intervals → Cost effectiveness, precision, low backlash, safety, environment-friendly machining → High-quality standards, production flexibility
<ul style="list-style-type: none"> • Pinion teeth with full helix modification • Involute profile and helix modification calculated and produced according to the operating load conditions • High quality output pinion gear designed to specifications 		<ul style="list-style-type: none"> → Improvement in contact patterns and nominal rating, achieving an optimal ring gear-pinion engagement → Best fit following the major ring gear manufacturers recommendation
<ul style="list-style-type: none"> • High tech controlling instruments 		<ul style="list-style-type: none"> → High quality and reliability standards
<ul style="list-style-type: none"> • Low Temperature Environment features • UL compliance certificate 		<ul style="list-style-type: none"> → Conformity to most severe demands → Conformity to U.S.A. specifications

Features and Benefits

<ul style="list-style-type: none"> • IEC electrical yaw brake motor wound and set for the specific application • Anti-sticking design of the parking brake motor • Braking torque adjustment • Customized power supply 		<ul style="list-style-type: none"> → Complete one-supplier gearmotor package → Constant braking performance → Protection of the drive from external overloads, where as the customized winding protects the drive from motor overloads → Simple machine design and achievement of more flexibility
<ul style="list-style-type: none"> • F.E.M. 1.001 ratings 		<ul style="list-style-type: none"> → Easy selection in according to class of mechanism
<ul style="list-style-type: none"> • Main certifications available, as: <ul style="list-style-type: none"> - ISO 9001 and 14000; - ATEX; - UL CSA; - Germanischer Lloyds. 		<ul style="list-style-type: none"> → Flexibility and adaptability to specific project needs
<ul style="list-style-type: none"> • Competent assistance and technical support during design/seletion activities 		<ul style="list-style-type: none"> → Professional pre-sale service → Calculation and selection tools → Selection optimization: performance, reliability, cost-efficiency
<ul style="list-style-type: none"> • Global service 		<ul style="list-style-type: none"> → Direct worldwide sales and service network
<ul style="list-style-type: none"> • 3 year warranty 		<ul style="list-style-type: none"> → The reliability of a quality product made to last → 3 year warranty since 1997

Quick selection (L2 T5), $n_2 = 15 \text{ min}^{-1}$

Quick selection

Table 1

Gear reducer size	Torques [N m] ¹⁾		Radial Loads [N] ^{1) 2)}			
	M_{N2} Dynamic torque (FEM L2 T5)	M_{2stat} Static torque	F_{r2} Dynamic radial load (FEM L2 T5)		$F_{r2,stat}$ Static radial load	
			GR Type	H Type	GR Type	H Type
100	1 500	2 200	62 000	25 800	100 000	46 500
200	2 700	4 000	62 000	-	100 000	-
300	4 000	5 000	56 400	56 400	117 500	117 500
500	6 500	10 000	56 400	56 400	117 500	117 500
800	10 000	15 000	73 000	77 400	140 000	148 000
1000	12 000	20 000	153 000	-	275 000	-
1300	15 000	30 000	180 000	180 000	312 500	312 500
2000	25 000	40 000	180 000	180 000	312 500	312 500
3000	30 000	72 000	298 000	-	700 000	-
4000	44 000	83 000	298 000	-	700 000	-
6000	72 000	120 000	415 000 ³⁾	-	910 000 ³⁾	-
8000	100 000	200 000	575 600 ³⁾	-	1 400 000 ³⁾	-
10000	125 000	250 000	666 200 ³⁾	-	1 700 000 ³⁾	-

1) For higher values, contact us.

2) Values according to ISO 281, valid for overhung loads acting in the middle of the pinion facewidth «b» (table 6).

3) See minimum value of dimension «G₁» (table 6).

Actual transmission ratios i

Table 2

Train of gear	Nominal transmission ratio i_N	Actual transmission ratio i Gear reducer size												
		100	200	300	500	800	1000	1300	2000	3000	4000	6000	8000	10000
3 stages	50	50,5	50,5	50,5	50,5	53,1	53,1	50,1	50,1	55,2	49,1	55,2	54,1	48,1
	60	59,6	59,6	59,6	59,6	62,6	62,6	59,1	59,1	62,0	58,6	65,9	64,6	57,4
	71	70,2	70,2	70,2	70,2	73,7	73,7	69,6	69,6	73,1	69,0	74,0	72,5	68,5
	85	86,6	86,6	86,6	86,6	92,4	92,4	87,2	-	91,6	86,5	85,4	83,7	87,9
	100	102	102	102	102	107	107	101	-	106	100	103	107	113
	125	128	128	128	128	134	134	127	-	123	129	132	129	134
	150	149	149	149	149	156	156	147	-	-	-	156	153	159
	180	179	179	179	179	189	189	178	-	-	-	192	-	-
	212	217	217	211	211	222	222	-	-	-	-	-	-	-
	250	255	255	-	-	-	-	-	-	-	-	-	-	-
300	301	301	-	-	-	-	-	-	-	-	-	-	-	
4 stages	212	-	-	-	-	-	-	-	-	-	205	231	226	201
	250	-	-	-	-	258	258	259	-	256	242	259	254	240
	300	-	-	290	290	304	304	301	-	302	285	305	299	282
	355	-	-	357	357	375	375	354	-	378	357	382	375	354
	425	-	-	421	421	442	442	418	418	439	414	444	435	411
	500	-	-	528	528	535	535	523	523	550	519	512	502	527
	600	-	-	613	613	670	670	608	608	638	603	615	644	677
	710	-	-	740	740	778	778	734	734	771	728	743	779	818
	850	-	-	894	894	974	974	887	887	890	934	953	934	970
	1 000	-	-	1 120	1 120	1 177	1 177	1 111	-	1 075	1 129	1 131	1 109	1 151

Selection, verifications and designation

Selection according to FEM 1.001¹⁾

Required application data

- Group and class of utilization (see tab. 5 as a guidance) for the mechanism involved.
- Load spectrum of the required torque and speed.
- Running conditions (accelerations-decelerations, frictional forces, wind effect).
- External drive data (pinion and ring-gear number of teeth and module).
- Gear reducer input speed (depending on motor type).

Required torque

Starting from running conditions (accelerations-decelerations, frictional forces, wind effect) and load spectrum determine the maximum load:

$$S_M = \max(S_{M \max I}; S_{M \max II})$$

where:

$$S_{M \max I} = (S_{MF} + S_{MA}) \cdot \gamma_m$$

is the maximum torque (combination of the most unfavourable actual values) during normal service without wind

$$S_{M \max II} = (S_{MF} + S_{MA} + S_{MW8}) \cdot \gamma_m$$

$$S_{M \max II} = (S_{MF} + S_{MW25}) \cdot \gamma_m$$

is the maximum of the two torque values (each one as a combination of the most unfavourable actual values) during normal service with wind

- S_{MF} is mean torque generated by friction;
- S_{MA} is mean torque generated by acceleration or deceleration;
- S_{MW8} is mean torque corresponding to a 80 N/m² wind;
- S_{MW25} is mean torque corresponding to a 250 N/m² wind;
- γ_m load amplification factor depending to mechanism group according to the following table:

Load amplification factor	Mechanism group							
	M1	M2	M3	M4	M5	M6	M7	M8
γ_m	1	1,04	1,08	1,12	1,16	1,2	1,25	1,3

Determine the gear reducer required output torque, as follows:

$$M_2 \text{ required} = S_M / (i_e \cdot \eta_e)$$

where:

- i_e is the external drive gear ratio (given by z_2 / z_1 , being z_1 and z_2 the number of teeth of the pinion and of the ring gear respectively)
- η_e is the the external drive efficiency (approx. 0,85)

Gear reducer size and transmission ratio selection

Select in the selection table (see tab. 6) a gear reducer size (also, the train of gears and the nominal transmission ratio i_N at the same time) on the basis of $n_2 \text{ max}$, $n_1 \text{ max}$, such as:

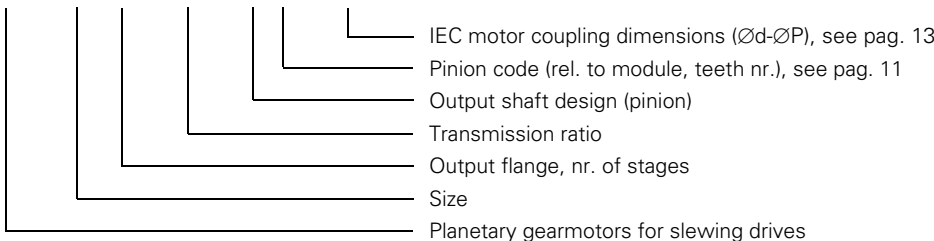
$$M_{N2} \geq M_2 \text{ required} \cdot K_A$$

$$i \geq i_{\text{required}}$$

1) For complete selection please refer to FEM section I 3rd edition.

Designation example:

EPS 1300 H3 - 850 - R xx - 19-200



Also available, on request:

- right angle shaft gear reducer;
- 5 stages gear reducer.

where:

- M_{N2} [N m] is the gear reducer nominal torque referred to FEM load spectrum class L2 and utilization class T5 (see tab. 3);
- K_A is the application factor (see tab. 4) which converts the gear reducer required torque according to the actual class of utilization and load spectrum;
- $n_2 \text{ max}$ [min-1] is the maximum speed required at the gear reducer low speed shaft ($n_2 \text{ application max} \cdot i_e$);
- $n_1 \text{ max}$ [min-1] is the maximum gear reducer input speed (depending on motor type; eg.: for a IEC 4 poles motor, $n_1 = 1\,400 \text{ min}^{-1}$);
- i_{required} gear reducer required transmission ratio ($n_1 \text{ max} / n_2 \text{ max}$).

Verifications

Radial load

Verify that the radial load on the gear reducer output pinion shaft when adjusted to spectrum class L2 and utilization class T5, is less than the reference value F_{r2} given in tab. 1;

$$\frac{M_2 \text{ required} \cdot K_A \cdot 2000}{D_p \cdot \cos \alpha} \leq F_{r2}$$

where:

- D_p [mm] is the permissible pinion pitch diameter;
- α [rad] pinion tooth pressure angle;
- F_{r2} [N] is the permissible radial load (L2 T5, $n_2 = 15 \text{ min}^{-1}$) acting in the middle of the pinion facewidth and without axial load.

Dynamic overloads

Starts on full load (especially for high inertiae and low transmission ratios), brakings, shocks, cases of gear reducers where the low speed shaft becomes motor due to the inertiae of driven machine, usually generate overloads. In these cases it is necessary to verify that the maximum peak torque is always lower than $M_{2 \text{ max}}$ (see tab. 3).

$$M_2 \text{ start} = \left(\frac{M_{\text{start}}}{M_N} \cdot M_2 \text{ available} - M_2 \text{ required} \right) \cdot \frac{J}{J + J_0} + M_2 \text{ required} \leq M_{2 \text{ max}}$$

$$M_2 \text{ brake} = \left(\frac{M_t}{\eta} \cdot i + M_2 \text{ required} \right) \cdot \frac{J}{J + J_0} - M_2 \text{ required} \leq M_{2 \text{ max}}$$

where:

- $M_2 \text{ max}$ [N m] is maximum dynamic torque;
- $M_2 \text{ available}$ [N m] is output torque due to the motor's nominal power;
- M_t [N m] is the braking torque at the gear reducer input shaft
- M_{start} / M_N is the ratio of motor peak.
- J_0 [kg m²] is the moment of inertia (of mass) of the motor;
- J [kg m²] is the external moment of inertia (of mass: coupling, driven machine, ect) referred to the motor shaft,
- η is the gear reducer efficiency: $\approx 0,91$ (3 stages) or $\approx 0,88$ (4 stages).

NOTE: when seeking to verify that starting torque is sufficiently high for starting, take into account starting friction, if any, in evaluating $M_2 \text{ required}$.

Static load

Verify that the gear reducer static torque and static radial load (see tab.1) are higher than static braking torque, and static overhung load (referred to the gear reducer low speed shaft):

$$M_2 \text{ stat} \geq M_t \cdot i / \eta$$

$$F_{r2 \text{ stat}} \geq \frac{M_t \cdot i \cdot 2000}{\eta \cdot D_p \cdot \cos \alpha}$$

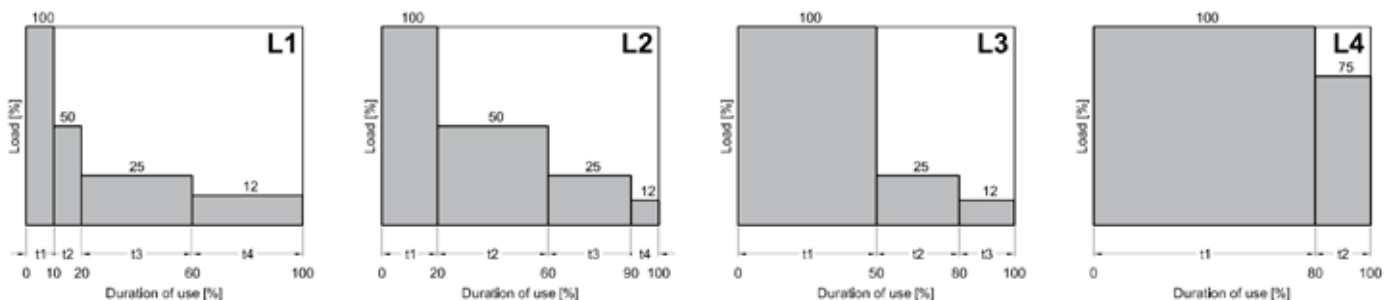
Application factor K_A and classification guidance

Application factors K_A and mechanism groups

Table 4

Class of load spectrum	Class of utilization						
	T2 400h < T2 ≤ 800h	T3 800h < T3 ≤ 1 600h	T4 1 600h < T4 ≤ 3 200h	T5 3 200h < T5 ≤ 6 300h	T6 6 300h < T6 ≤ 12 500h	T7 12 500h < T7 ≤ 25 000h	T8 25 000h < T8 ≤ 50 000h
L1 $0 < K_m \leq 0,125$	M1 0,75	M2 0,80	M3 0,86	M4 0,93	M5 1,00	M6 1,08	M7 1,16
L2 $0,125 < K_m \leq 0,25$	M2 0,81	M3 0,87	M4 0,93	M5 1,00	M6 1,08	M7 1,16	M8 1,26
L3 $0,25 < K_m \leq 0,5$	M3 0,89	M4 0,96	M5 1,03	M6 1,11	M7 1,19	M8 1,29	M8 1,38
L4 $0,5 < K_m \leq 1$	M4 0,97	M5 1,04	M6 1,12	M7 1,21	M8 1,30	M8 1,40	M8 1,51

Load spectra (examples)



Group classification guidance

Table 5

Type of appliance Designation	Particulars concerning nature of use	Type of mechanism				
		Slewing	Hoisting	Luffing	Traverse	Travel
Erection cranes	-	M2 – M3	M2 – M3	M1 – M2	M1 – M2	M2 – M3
Stocking and reclaiming transporter	Hook duty	M4	M5 – M6	-	M4 – M5	M5 – M6
Stocking and reclaiming transporter	Grab or magnet	M6	M7 – M8	-	M6 – M7	M7 – M8
Workshop cranes		M4	M6	-	M4	M5
Overhead travelling cranes, pigbreaking cranes, scrapyard cranes	Grab or magnet	M6	M8	-	M6 – M7	M7 – M8
Bridge cranes for unloading, bridge cranes for containers Other bridge cranes (with crab and/or slewing jib crane)	a) Hook or spreaded duty d) Hook duty	M5 – M6 M4 – M5	M6 – M7 M4 – M5	M3 – M4 -	M6 – M7 M4 – M5	M4 – M5 M4 – M5
Bridge cranes for unloading, bridge cranes (with crab and/or slewing jib crane)	Grab or magnet	M5 – M6	M8	M3 – M4	M7 – M8	M4 – M5
Drydock cranes, shipyard jib cranes, jib cranes for dismantling	Hook duty	M4 – M5	M5 – M6	M4 – M5	M4 – M5	M5 – M6
Dockside cranes (slewing, on gantry, etc.), floating cranes and pontoon derricks	Hook duty	M5 – M6	M6 – M7	M5 – M6	-	M3 – M4
Dockside cranes (slewing, on gantry, etc.), floating cranes and pontoon derricks	-	M6 – M7	M7 – M8	M6 – M7	-	M4 – M5
Floating cranes and pontoon derricks for very heavy loads (usually greater than 100t)	-	M3 – M4	M3 – M4	M3 – M4	-	
Deck cranes	Hook duty	M3 – M4	M4	M3 – M4	M2	M3
Deck cranes	Grab or magnet	M3 – M4	M5 – M6	M3 – M4	M4 – M5	M3 – M4
Tower cranes for building	-	M5	M4	M4	M3	M3
Derricks	-	M1 – M2	M2 – M3	M1 – M2	-	-
Railway cranes allowed to run in train	-	M2 – M3	M3 – M4	M2 – M3	-	-
Mobil cranes	Hook	M2 – M3	M3 – M4	M2 – M3	-	-

Dimensions

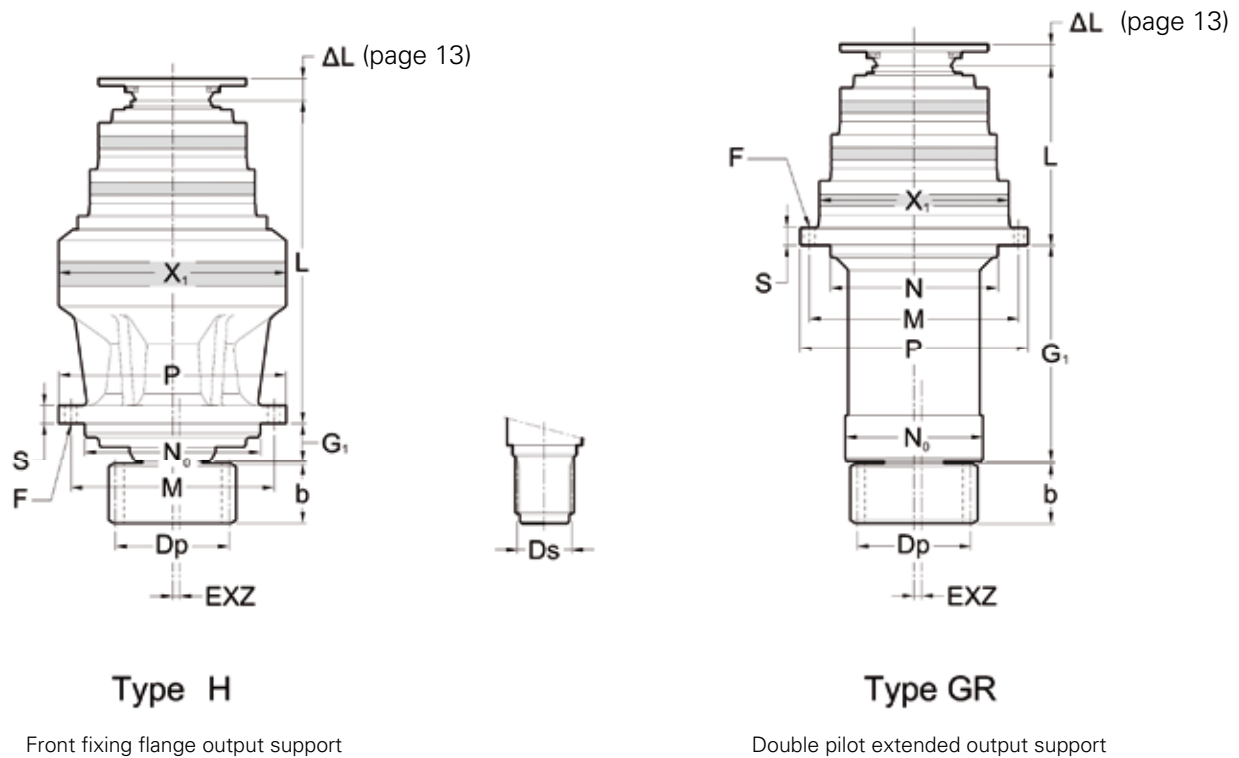
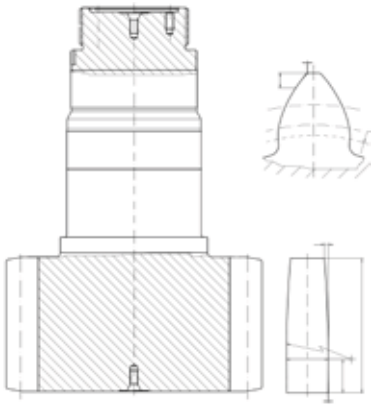


Table 6

EPS Gear reducers		Dimensions											Output pinion shaft			
		D _s	F ∅×nr. mm	G ₁	M ∅ mm	N ∅ mm	N ₀ ∅ mm	P ∅ mm	S mm	X ₁ ∅ mm	L mm		module mm	b facewidth mm	Dp _{min} ∅ mm	EXZ mm
size	type									3 stages	4 stages					
		DIN 5482 E9														
100	H	50×45	10,5 _{x8}	6	165	–	110 f7	185	12	200	232	282	5 – 6	56	80	–
100	GR	58×53	10,5 _{x4}	162	240	160 h6	150 h6	275	32	200	176,5	226,5	5 – 6	68	98	0,5
200	GR	58×53	17,5 _{x4}	162	240	160 h6	150 h6	275	32	200	188,5	238,5	6 – 8	68	98	0,5
300	H	70×64	12,5 _{x10}	39	245	–	175 f7	272	20	240	279	329	6 – 8	90	110	–
300	GR	70×64	10,5 _{x8}	142	224	200 g7	195 g7	244	63	240	176	226	8	90	110	–
500	H	70×64	12,5 _{x10}	40	245	–	175 f7	272	20	240	306	356	8 – 10	90	120	–
500	GR	70×64	10,5 _{x8}	142	224	200 g7	195 g7	244	78	240	203	253	8 – 10	90	120	–
800	H	80×74	17 _{x12}	40	250	–	200 f7	280	22	280	349	399	10 – 12	90	120	–
800	GR	80×74	12,5 _{x10}	184	260	240 g7	200 g7	280	80	280	205	255	10 – 12	90	120	–
1000	GR	100×94	17 _{x16}	303	350	278 g7	228 g7	380	30	315	205,5	255,5	12	110	160	0,75
1300	H	100×94	16,5 _{x20}	57	295	–	250 f7	325	30	353	416,5	466,5	12 – 14	110	160	–
1300	GR	100×94	17 _{x18}	233	325	290 g7	250 g7	363	96	363	240,5	290,5	12 – 14	110	160	1,5
2000	H	100×94	17 _{x18}	57	295	–	250 f7	325	30	353	438,5	488,5	12 – 14 – 16	110	160	–
2000	GR	100×94	17 _{x18}	233	325	290 g7	250 g7	363	118	363	262,5	312,5	12 – 14 – 16	110	160	0,5
		DIN 5480 9H														
3000	GR	140×5	22 _{x24}	355 min 1 855 max	475	430 h7	340 h7	515	40	428	341	383,5	16 – 18 – 20	150	224	2,5 – 5
4000	GR	140×5	22 _{x24}	355 min 1 855 max	475	430 h7	340 h7	515	40	428	362	416,5	16 – 18 – 20	150	224	2,5 – 5
6000	GR	160×5	26 _{x24}	355 min 1 855 max	525	465 h7	340 h7	575	45	445	406	460,5	16 – 18 – 20	150	300	2,5 – 5
8000	GR	200×5	26 _{x24}	710 min 1 810 max	630	580 h7	510 h7	690	50	542	335,5	403,5	20 – 22	170	300	5
10000	GR	200×5	33 _{x24}	730 min 1 830 max	680	630 h7	510 h7	740	50	542	335,5	403,5	20 – 22 – 24	170	300	5

Installation and lubrication

Output pinion



Design features:

- full helix modification
- ground finish
- tip relief
- gear accuracy grade DIN 8
- addendum modification coefficient $x = 0,5$

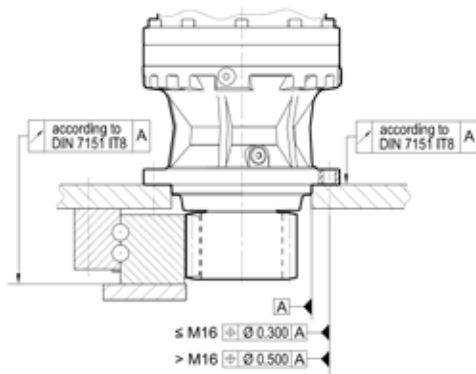
	Module													
	5	6	7	8	9	10	11	12	14	16	18	20	22	24
Code for designation	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z

	Nr. of teeth																						
	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
Code for designation	A	B	C	D	E	F	G	H	I	K	L	M	N	O	P	Q	R	S	T	U	V	W	X

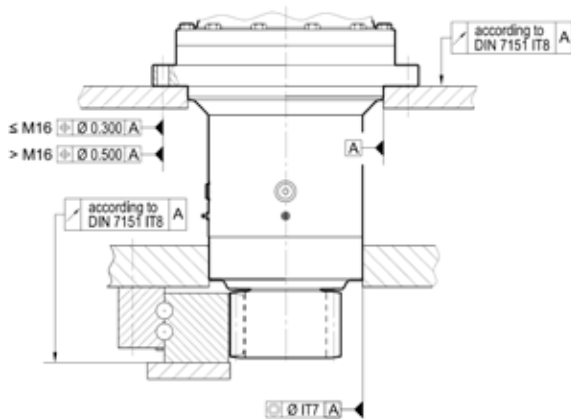
Pinion designation example: R **PC** (pinion with $m = 8$, $z = 12$), see also page 8.

Installation

To ensure proper functioning and optimum transfer of power between the gear reducers and the driven gear, the gear reducers requires a rigid connection construction that is resistant to torsion. The form and position tolerances listed below must be met.



Dimension tolerances of the assembly construction for slewing gear reducers



Dimension tolerances of the assembly construction for slewing gear reducers

Lubrication

The main lubricant manufacturers as well as the ISO viscosity grade to be used are stated in the following tables. Use only lubricants with **EP** (extreme pressure) **additives**.

Polyglycol basis synthetic lubricants may **not mixed** with other type's lubricants (mineral and PAO lubricants). Before any lubricant type change, carefully clean the gear reducer.

Never mix different makes of synthetic oil; if oil-change involves switching to a type different from that used hitherto, then give the gear reducer a through clean-out.

Manufacturer	PAO synthetic oil ISO VG 150 ... 460	mineral oil ISO VG 150 ... 460
AGIP	Blasia SX 220 ... 460	Blasia
ARAL	Degol PAS	Degol BG
BP	Energyn EPX	Energol GR XP
KLÜBER	Klübersynth GEM4	Klüberoil GEM1
MOBIL	Mobilgear SHC XMP	Mobilgear 600 XP Mobilgear XMP
SHELL	Omala HD	Omala
TOTAL	Carter EP SH	Carter EP

ISO viscosity grade

Mean kinematic viscosity [cSt] at 40 °C.

Speed n_2 min ⁻¹	Ambient temperature ¹⁾ [°C]	
	mineral oil 0 ÷ 20	10 ÷ 40
> 140	150	220
140 ÷ 2,0	220	320
< 2,0	320	460

1) Peaks ± 10°C are acceptable.

Oil temperature [°C]	Oil-charge interval [h]	
	synthetic oil	mineral oil
≤ 65	12 500	5 600
65 ÷ 80	9 000	2 800
80 ÷ 95	6 300	1 400

Oil-change intervals assume pollution-free surroundings. When heavy overloads are present, halve the values.

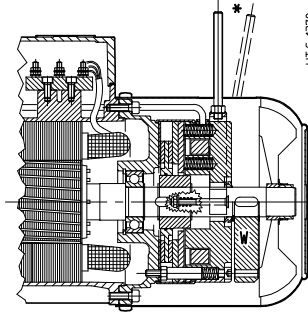
Independently from running times, change the oil as follows:

- every 1 ÷ 2 years, for mineral oil;
- every 2 ÷ 4 years, for synthetic oil.

Electric motor

HBZ

Asynchronous three-phase **brake motor** with **d.c. brake**



UTC 1370

Thanks to its high **quietness**, **progressivity** and **dynamic** characteristics, it is specifically suitable for **coupling with gearmotor minimizing the dynamic overloads** deriving from **starting and braking phases** (especially in case of motion reversals) and maintaining a **very good braking torque value**.

The excellent **operation progressivity** - when starting and braking - is assured by the brake anchor which is less quick in the impact (compared to a.c. HBF types) and by the slight quickness of d.c. brakes.

Offering a comprehensive **range of accessories and non-standard designs** in order to satisfy all possible gearmotor application fields (e.g. IP 56, IP 65, flywheel, encoder, independent cooling fan, independent cooling fan and encoder, double extension shaft, integrated motor-inverter, etc.).

* on request.

Multi-voltage brake rectifier

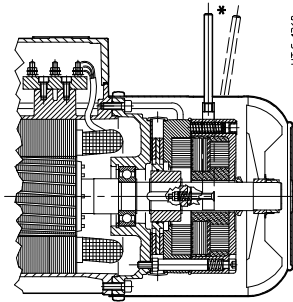


Multi-voltage brake rectifier (patent pending) which generates a preset constant output voltage independent from input supply (and from its fluctuations) and, compared to a usual rectifier, reduces the voltage to keep the brake released.

- Possibility to supply the brake at 230, 400 or 460 V a.c. indifferently;
- Higher steadiness of brake characteristics, lower energy consume, lower coil heating and lower braking delay;
- No special brake coil;
- Ready to use in NEMA environment;
- Max availability and stock flexibility.

HBF

Asynchronous three-phase **brake motor** with **a.c. brake**



UTC 1368

The **high reactivity** typical of **a.c. brake** and the **high braking capacity** make this brake motor **particularly suitable for heavy duties** requiring **quick brakings** and a **high number of operations** (e.g.: lifts with high frequency of starting, usually for size > 132, and/or for jog operations).

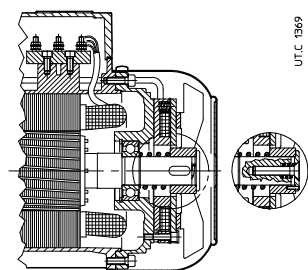
Vice versa, its very **high dynamic characteristics** (rapidity and frequency of starting) **are not advisable for the use in gearmotor coupling**, especially when these features are not strictly necessary for the application (avoiding useless overloads on the whole transmission).

Comprehensive **range of accessories and non-standard designs** in order to satisfy all application needs of gearmotors (in particular for HBF: IP 56, IP 65, encoder, independent cooling fan, independent cooling fan and encoder, double extension shaft, integrated motor-inverter, etc.).

* on request.

HBV

Asynchronous three-phase **brake motor** with **d.c. safety brake**

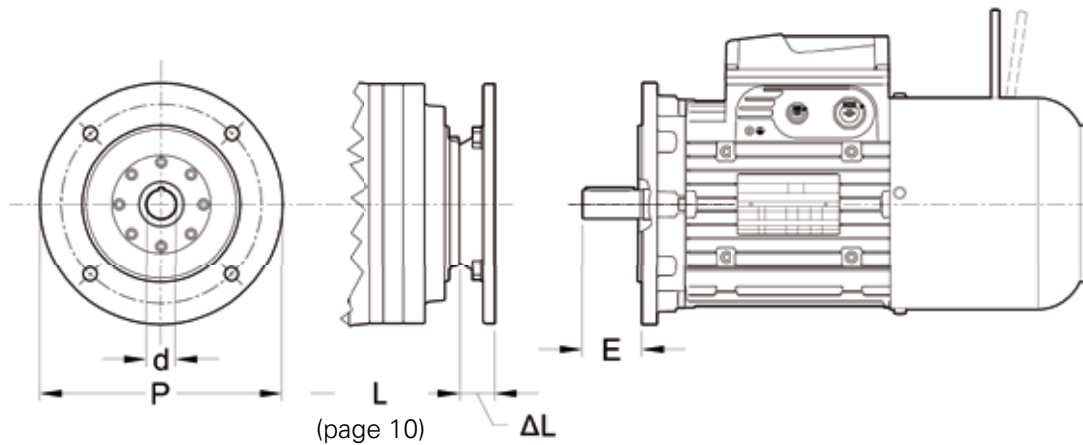


UTC 1369

Featuring **maximum economy**, **very reduced overall dimensions and moderate braking torque**, it is suitable for the coupling with gearmotor and can be applied as brake for **safety or parking stops** (e.g. cutting machines) and for operations at deceleration ramp end **during the running with inverter**.

The standard cast iron fan supplies a flywheel effect increasing the very good progressivity of starting and braking (typical of d.c. brake) being particularly **suitable for «light» traverse movements**.

Electric motor



Motor size	Main coupling dimensions UNEL 13117-71 (DIN 42677 BI 1.A-65, IEC 72.1)	
	Shaft end Ø d × E	Flange Ø P B5
63	11 × 23	140
71	14 × 30	160
80,90 B5R	19 × 40	200
90, 100 B5R, 112 B5R	24 × 50	200
100, 112, 132 B5R	28 × 60	250
132, 160 B5R	38 × 80	300
160	42 × 110	350
180, 200 B5R	48 × 110	350
200	55 × 110	400
225, 250 B5R	60 × 140	450
250	65 × 140	550
280, 315S B5R	75 × 140	550
315	80 × 170	660

Train of gear	IEC frame size	P Ø	d Ø	Gear reducer size length variation ΔL													
				100	200	300	500	800	1000	1300	2000	3000	4000	6000	8000	10000	
3 stages	56	120	9	20	-	-	-	-	-	-	-	-	-	-	-	-	-
	63	140	11	20	20	-	-	-	-	-	-	-	-	-	-	-	-
	71	160	14	20	20	20	-	-	-	-	-	-	-	-	-	-	-
	80	200	19	30	30	30	-	-	-	-	-	-	-	-	-	-	-
	90	200	24	30	30	30	30	30	30	30	48	48	61	61	61	-	-
	100, 112	250	28	48	48	48	30	30	48	48	48	61	61	61	61	-	-
	132	300	38	-	-	-	48	61	61	61	127	127	127	127	-	-	-
	160	350	42	-	-	-	61	127	127	127	127	127	127	127	-	-	-
	180	350	48	-	-	-	-	-	-	-	-	-	127	127	-	-	-
	200	400	55	-	-	-	-	-	-	-	-	-	145	145	198	-	-
225	450	60	-	-	-	-	-	-	-	-	-	-	145	198	-	-	
250	550	65	-	-	-	-	-	-	-	-	-	-	-	198	198	198	
4 stages	56	120	9	20	20	20	20	-	-	-	-	-	-	-	-	-	-
	63	140	11	20	20	20	20	20	20	20	20	20	20	20	20	20	20
	71	160	14	20	20	20	20	20	20	20	20	20	20	20	20	20	20
	80	200	19	-	30	30	30	30	30	30	30	30	30	30	30	-	-
	90	200	24	-	-	-	30	30	30	30	30	30	48	48	48	48	48
	100, 112	250	28	-	-	-	-	48	48	48	48	-	61	61	61	61	61
	132	300	38	-	-	-	-	-	-	-	-	-	127	127	127	127	127
	160	350	42	-	-	-	-	-	-	-	-	-	127	127	127	127	127
	180	350	48	-	-	-	-	-	-	-	-	-	-	-	-	127	127
	200	400	55	-	-	-	-	-	-	-	-	-	-	-	-	145	145
225	450	60	-	-	-	-	-	-	-	-	-	-	-	-	-	145	
250	550	65	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

Application data template



Customer :

Application description:

Mechanism (FEM 1.001 1998.10.01):

FEM Class: **M** _____
 Load Spectrum Class: **L** _____
 Running time Class: **T** _____

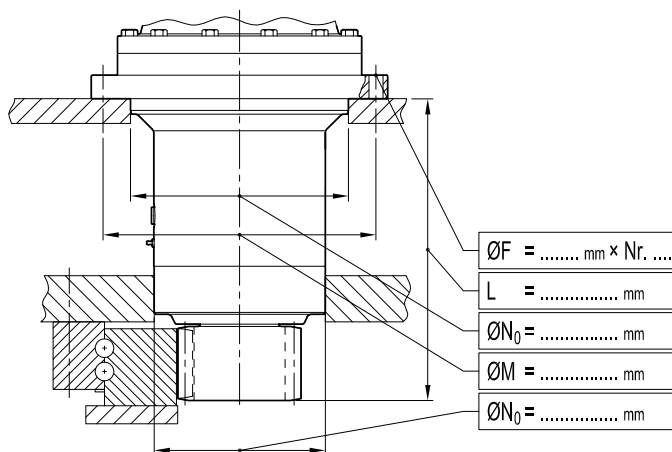
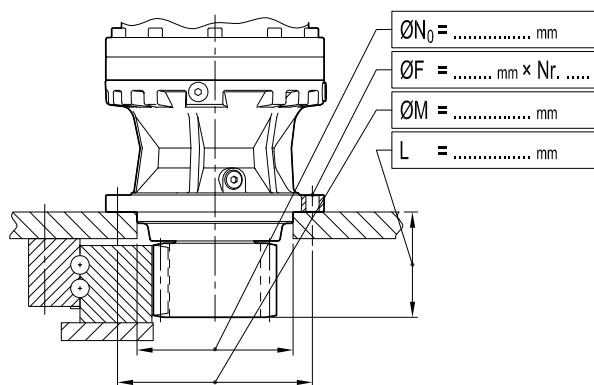
Torques at pinion:

Output torque at pinion $M_{N2required}$ _____ [N m]
 Has γ_m factor been included in $M_{N2required}$ yes no
 Peak / Static torque at pinion M_{2stat} _____ [N m]
 Pinion speed n_2 _____ [min^{-1}]
 Maximum working angle (referrd to gearbox working position) _____ [°]

Relevant Geometry (please fill-out relevant dotted lines):

Type **H**

Type **GR**

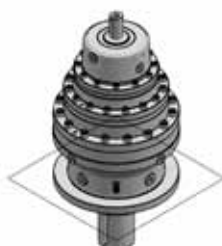


Mounting positions

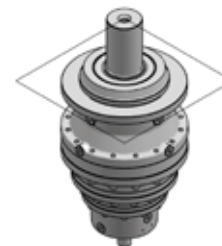
B5



V1



V3



Application data template



Slew gears data:

Centre distance (Pinion - Slew Ring) a: _____ [mm]

Pinion One piece solid
 Fitted on splined shaft

Slew Ring (Ring Bearing) Internal toothing
 External toothing

m modulus _____ [mm]

m modulus _____ [mm]

Z₁ N°. of teeth _____ [-]

Z₂ N°. of teeth _____ [-]

x-m profile correction _____ [mm]

x-m profile correction _____ [mm]

b₁ facewidth _____ [mm]

b₂ facewidth _____ [mm]

Material _____

Material _____

Heat treatment _____

Heat treatment _____

Hardness _____

Hardness _____

Electric Motor:

Power: _____ [kW]; Voltage: _____ [V]; Frequency: _____ [Hz]; N° poles: _____ [-];

Frequency Control device: yes no

Motor brake: yes no

Dynamic braking torque: _____ [N m] Static braking torque: _____ [N m]

Hydraulic Brake: yes no

Dynamic braking torque: _____ [N m] Static braking torque: _____ [N m]

Hydraulic Brake:

Brand and type: _____ Shaft type: _____

Displacement: _____ [cc]; Max pressure: _____ [MPa]; Working pressure: _____ [MPa];

Notes and Remarks: _____

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Index of revisions

List of updates (Cat. EPS - Edition April 2011 available on www.rossi-group.com)

Page 6: Updates quick selection table.

Page 14 Updated slewing drive datasheet.

List of updates (Cat. EPS - Edition December 2011 available on www.rossi-group.com)

Pag. 14, 15: Updates application data template.

History and know-how



For more than 50 years, Rossi has been developing its business in the most demanding applications to become one of the world's leading gearmotor manufacturers suitable for critical machines. Even in the toughest environment, Rossi is recognized for providing state of the art technology, solid value, and commitment to its customers.

Whatever gear reducer or gear motor your technology may need, Rossi's qualified staff is at your disposal to provide assistance, support, and innovative solutions during the design phase.

Customer tailored solutions may be found to maximize performance, while, at the same time, minimizing the overall machine cost.



More than:



- **50 years** of experience and success in the **power transmission** field
- **20 years** in **wind industry**
- **100 000 wind drives** installed

enables Rossi to offer Customers a comprehensive product range including helical, bevel, worm, planetary gear reducers and gearmotors; gear reducer for heavy applications, electric motors,

servomotors, inverters, servoinverters, and on board inverter drives.



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Product liability, application considerations

The Customer is responsible for the correct selection and application of product in view of its industrial and/or commercial needs, unless the use has been recommended by technical qualified personnel of Rossi, who were duly informed about customer's application purposes. In this case all the necessary data required for the selection shall be communicated exactly and in writing by the Customer, stated in the order and confirmed by Rossi. The Customer is always responsible for the safety of product applications. Every care has been taken in the drawing up of the catalog to ensure the accuracy of the information contained in this publication, however Rossi can accept no responsibility for any errors, omissions or outdated data. Due to the constant evolution of the state of the art, Rossi reserves the right to make any modification whenever to this publication contents. The responsibility for the product selection is of the customer, excluding different agreements duly legalized in writing and undersigned by the Parties.

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